

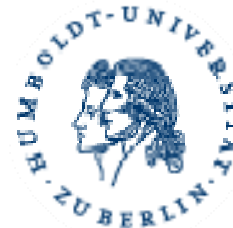


Constrained Single-Step One-Shot Method with Applications in Aerodynamics

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Collaborators

- **HU Berlin:** A. Griewank, A. Hamdi, E. Özkaya, A. Plocke
- **DLR:** C. Ilic
- **Uni Paderborn:** A. Walther
- **Uni Trier:** V. Schulz, S. Schmidt

Problem Statement



Goal: $\min_u f(y, u) \quad \text{s.t.} \quad c(y, u) = 0,$

where y and u are the state and design variables.

Given fixed point iteration $y_{k+1} = G(y_k, u)$ (e.g. pseudo-time stepping) to solve PDE $c(y, u) = 0$.

Assumptions:

- $\frac{\partial c}{\partial y}$ always invertible. IFT \Rightarrow given $u, \exists! y$ s.t. $c(y, u) = 0$.
- $G, f \in C^{2,1}$.
- G contractive: $\|G_y(y, u)\| = \|G_y^T(y, u)\| \leq \rho < 1$

One-Shot approach



$$L(y, \bar{y}, u) = f(y, u) + (G(y, u) - y)^T \bar{y}$$

$$= \underbrace{N(y, \bar{y}, u)} - y^T \bar{y}$$

shifted Lagrangian

Stationary point:

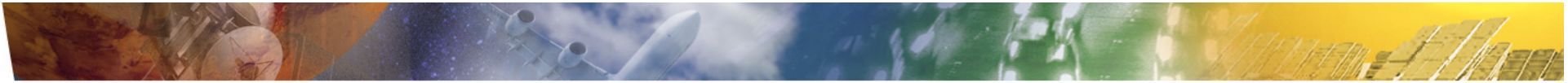
$$\begin{cases} L_{\bar{y}} = G(y, u) - y = 0 \\ L_y = N_y(y, \bar{y}, u)^T - \bar{y} = 0 \\ L_u = N_u(y, \bar{y}, u)^T = 0 \end{cases}$$

One-step one-shot (step $k+1$):

$$(OS) \begin{cases} y_{k+1} = G(y_k, u_k) & \text{primal update} \\ \bar{y}_{k+1} = N_y(y_k, \bar{y}_k, u_k)^T & \text{dual update} \\ u_{k+1} = u_k - B_k^{-1} N_u(y_k, \bar{y}_k, u_k)^T & \text{design update} \end{cases}$$

Aims: Choose B such that:

- **Convergence of (OS).**
- **Bounded retardation.**



Bounded retardation



Jacobian of the extended iteration:

$$J_* = \frac{\partial(y_{k+1}, \bar{y}_{k+1}, u_{k+1})}{\partial(y_k, \bar{y}_k, u_k)} \Big|_{(y^*, \bar{y}^*, u^*)} = \begin{pmatrix} G_y & 0 & G_u \\ N_{yy} & G_y^T & N_{yu} \\ -B^{-1}N_{uy} & -B^{-1}G_u^T & I - B^{-1}N_{uu} \end{pmatrix}$$

Whenever we can define B such that

$$\frac{1 - \rho(G_y)}{1 - \hat{\rho}(J_*)} < \text{const}$$

we have bounded retardation.

Necessary condition for contractivity



Eigenvalues of J_* are the zeros of the equation

$$\det((\lambda - 1)B + H(\lambda)) = 0$$

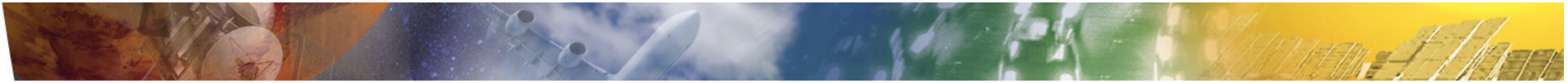
where

$$H(\lambda) = \begin{pmatrix} -G_u^T (G_y^T - \lambda I)^{-1}, I \end{pmatrix} \begin{pmatrix} N_{yy} & N_{yu} \\ N_{uy} & N_{uu} \end{pmatrix} \begin{pmatrix} -(G_y - \lambda I)^{-1} G_u \\ I \end{pmatrix}.$$

Necessary (but not sufficient) condition for contractivity:

$$B = B^T \succ 0 \quad \text{and} \quad B \succ \frac{1}{2} H(-1).$$

[Griewank, 2006]



Exact penalty function: L^a

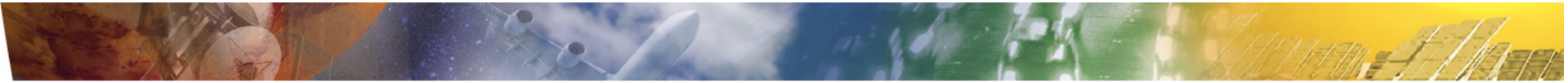
Remark:

Deriving (sufficient) conditions on B for J_* to have a spectral radius smaller than 1 has proven difficult.

Instead, we look for descent on the **augmented Lagrangian**

$$L^a(y, \bar{y}, u) := \underbrace{\frac{\alpha}{2} \|G(y, u) - y\|^2}_{\text{primal residual}} + \underbrace{\frac{\beta}{2} \|N_y(y, \bar{y}, u)^T - \bar{y}\|^2}_{\text{dual residual}} + \underbrace{N - \bar{y}^T y}_{\text{Lagrangian}},$$

where $\alpha > 0$ and $\beta > 0$.

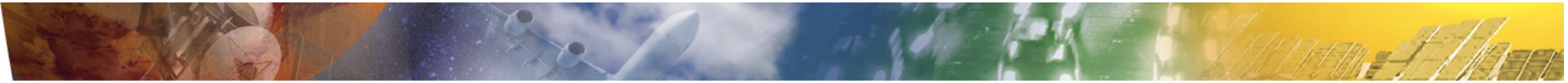


Correspondence condition

The full gradient of L^a is given by

$$\begin{bmatrix} \nabla_y L^a \\ \nabla_{\bar{y}} L^a \\ \nabla_u L^a \end{bmatrix} = -Ms(y, \bar{y}, u), \quad \text{where } s(y, \bar{y}, u) = \begin{bmatrix} G(y, u) - y \\ N_y(y, \bar{y}, u)^T - \bar{y} \\ -B^{-1}N_u(y, \bar{y}, u)^T \end{bmatrix}$$

$$\text{and } M = \begin{bmatrix} \alpha(I - G_y^T), & -I - \beta N_{yy}, & 0 \\ -I, & \beta(I - G_y), & 0 \\ -\alpha G_u^T, & -\beta N_{yu}^T, & B \end{bmatrix}.$$



Correspondence condition

Consequence (Correspondence condition):

There is a 1-1 correspondence between the stationary points of L^a and the roots of s if

$$\det[\alpha\beta(I - G_y^T)(I - G_y) - I - \beta N_{yy}] \neq 0,$$

for which it is sufficient that

$$\alpha\beta(1 - \rho)^2 > 1 + \beta \|N_{yy}\|.$$

[Hamdi, Griewank, 2008]

Descent condition



Theorem (Descent condition):

$s(y, \bar{y}, u)$ is a descent direction for all large positive B

if and only if

$$\alpha\beta\left(I - \frac{1}{2}(G_y + G_y^T)\right) > \left(I + \frac{\beta}{2}N_{yy}\right)\left(I - \frac{1}{2}(G_y + G_y^T)\right)^{-1}\left(I + \frac{\beta}{2}N_{yy}\right),$$

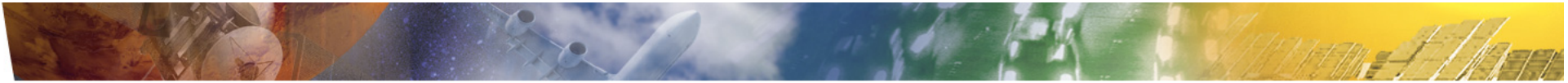
which is implied by $\sqrt{\alpha\beta}(1-\rho) > 1 + \frac{\beta}{2}\|N_{yy}\|$.

➤ Satisfied for $\beta = \frac{2}{c}$, $\alpha = \frac{2c}{(1-\rho)^2}$ with $c = \|N_{yy}\|$.

Theorem: A suitable B is given by:

$$B = \alpha G_u^T G_u + \beta N_{yu}^T N_{yu} + N_{uu}.$$

[Hamdi, Griewank, 2008]



One-step one-shot

Aerodynamic shape design

Descent for $\beta = \frac{2}{c}$, $\alpha = \frac{2c}{(1-\rho)^2}$ **with** $c = \|N_{yy}\|$.

(In practice choose $c = 1$, $\Rightarrow \beta = 2$, $\alpha \gg 1$.)

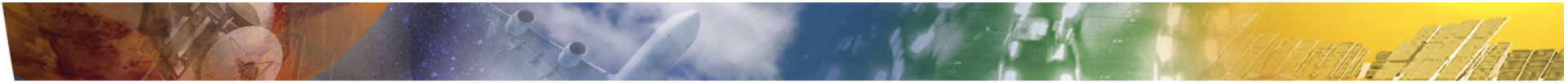
A suitable B **is given by** $B = \alpha G_u^T G_u + \beta N_{yu}^T N_{yu} + N_{uu}$.

Instead BFGS updates for the Hessian

$$\nabla_u^2 L^a = \underbrace{\alpha G_u^T G_u + \beta N_{yu}^T N_{yu} + N_{uu}}_B + \underbrace{\alpha (G - y)^T}_{\rightarrow *0} G_{uu} + \beta \underbrace{(N_y^T - \bar{y})^T}_{\rightarrow *0} N_{yuu}.$$

The gradient $\nabla_u L^a = \alpha (G - y)^T G_u + \beta (N_y - \bar{y})^T N_{yu} + N_u$

is evaluated by Algorithmic Differentiation (AD).

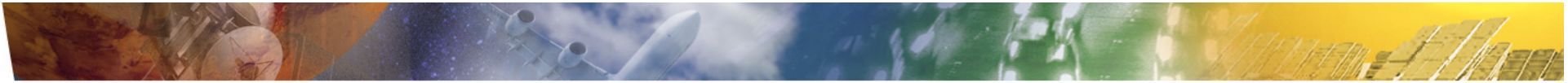


One-step one-shot

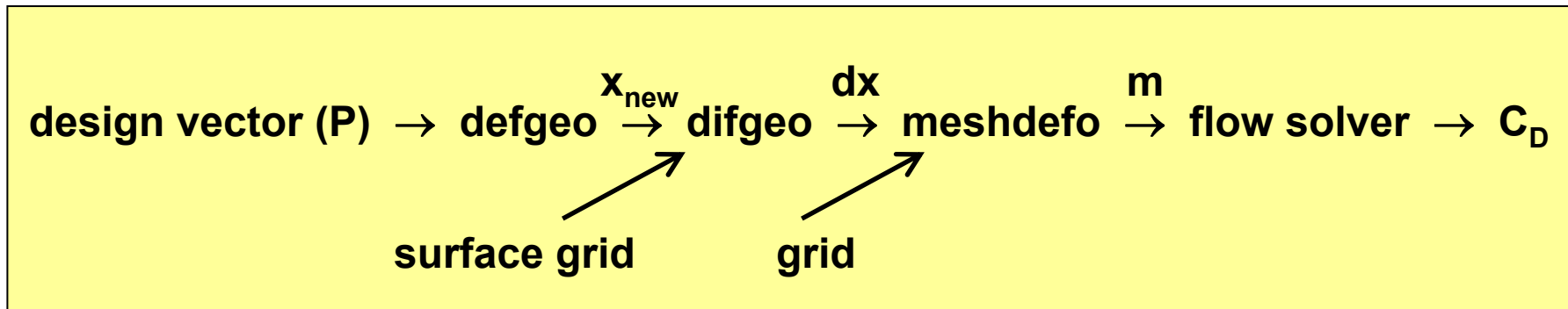
Aerodynamic shape design



- **Transonic case: RAE 2822 at $Ma = 0.73$ with $\alpha = 2^\circ$**
- **Cost function: drag (c_d)**
- **TAUij (2D Euler) + mesh deformation + parameterization**
- **First and second derivatives by AD tool ADOL-C**
- **Geometric constraint: constant thickness**
- **Camberline/Thickness decomposition,
20 Hicks-Henne coefficients define camberline**



Automatic Differentiation of Entire Design Chain



- Adjoint version of entire design chain by **ADOL-C**
- TAUij (2D Euler) + mesh deformation + parameterization

$$\frac{dC_D}{dP} = \frac{\partial C_D}{\partial m} \cdot \frac{\partial m}{\partial(dx)} \cdot \frac{\partial(dx)}{\partial x_{new}} \cdot \frac{\partial x_{new}}{\partial P} \quad \text{and} \quad \frac{\partial(dx)}{\partial x_{new}} = \frac{\partial(x_{new} - x_{old})}{\partial x_{new}} = Id$$

↑ ↑ ↑
TAUij_AD meshdefo_AD defgeo_AD

One-step one-shot

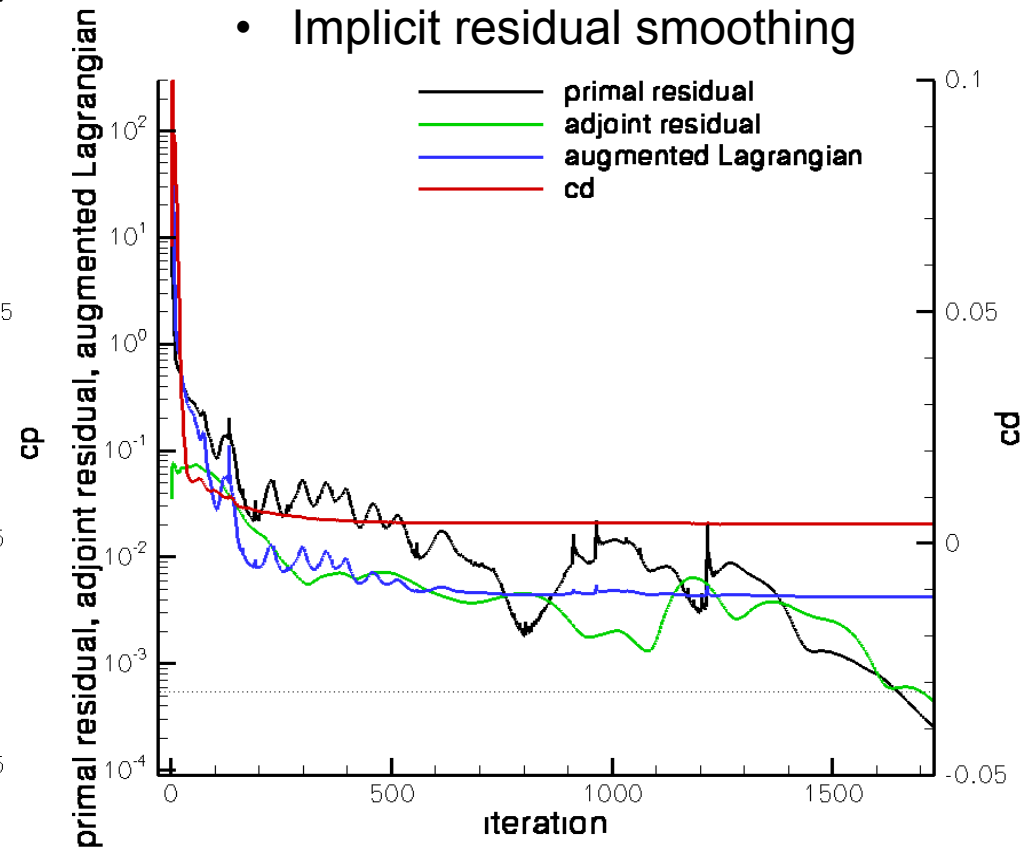
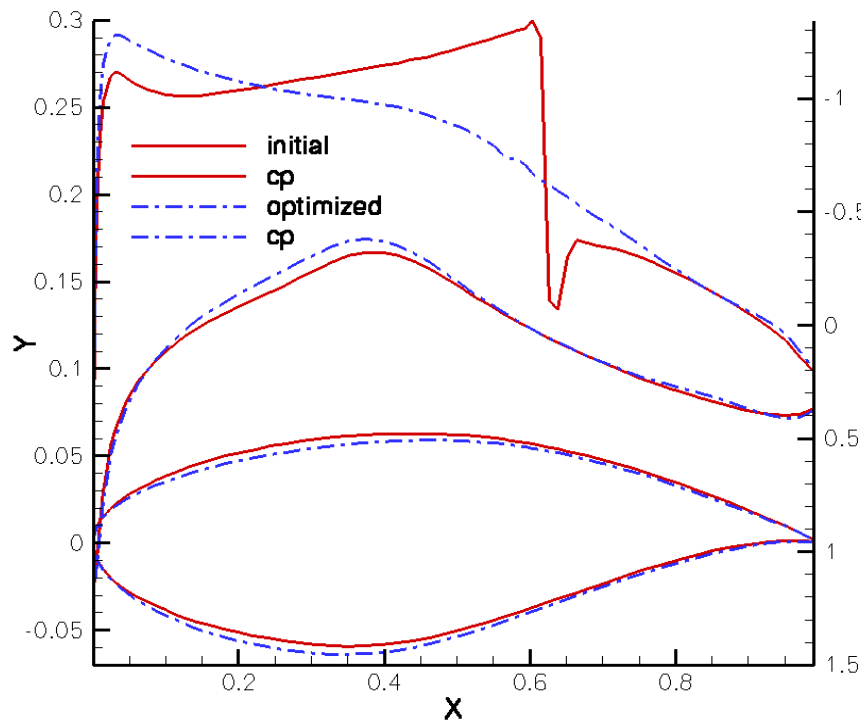


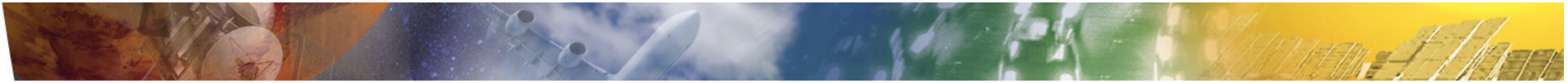
Drag reduction

- RAE 2822, $M = 0.73$, $\alpha = 2.0^\circ$
- inviscid flow, mesh 161x33 cells
- 20 design variables (Hicks-Henne)
- One-step one-shot

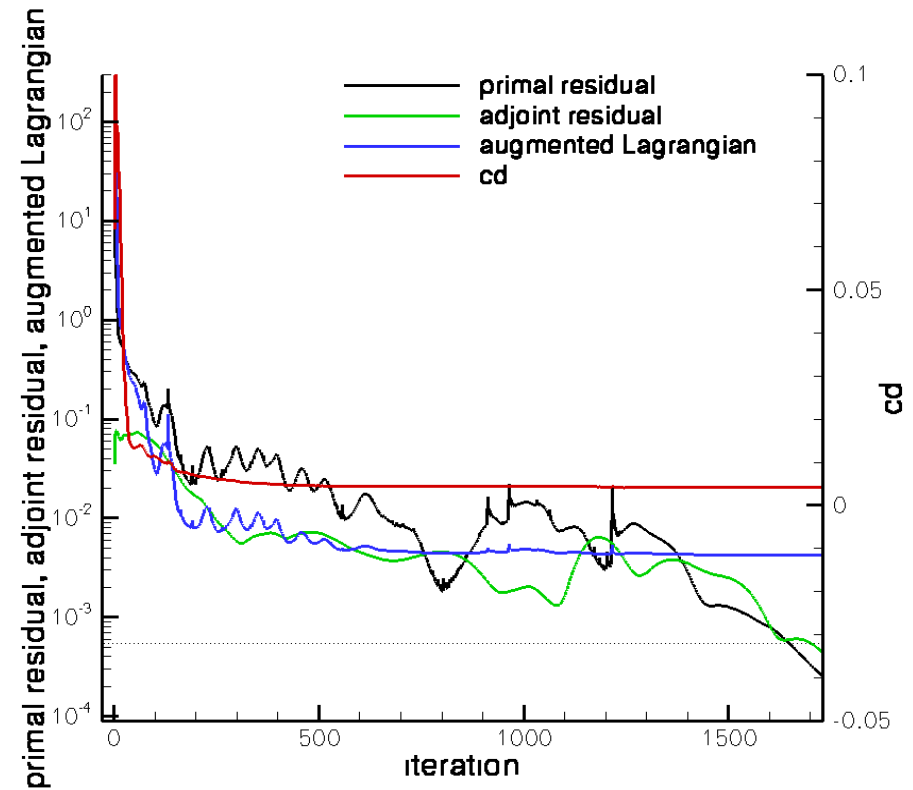
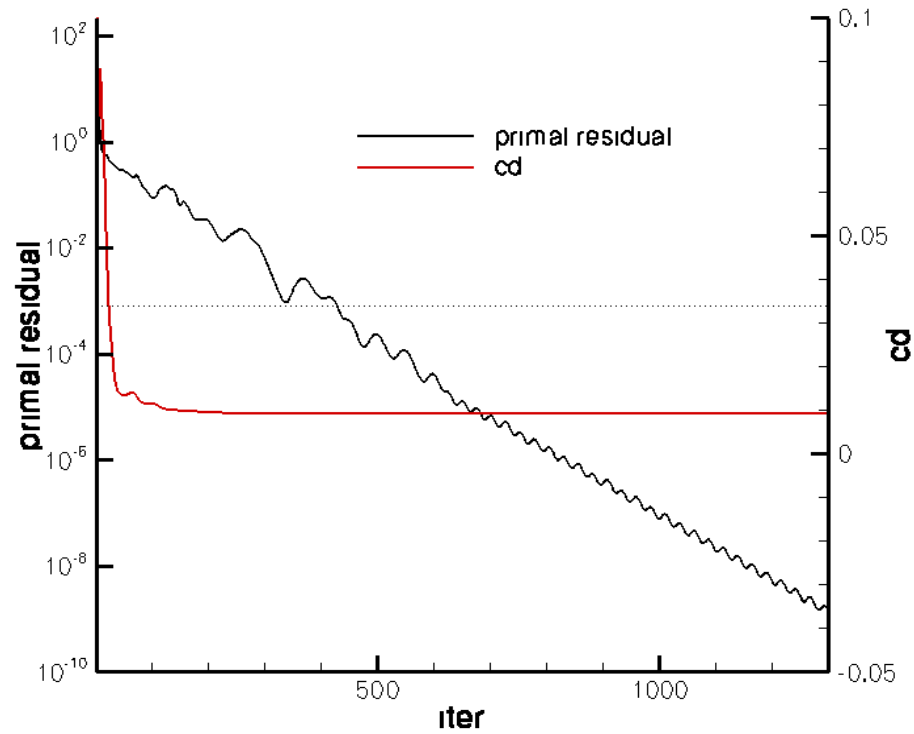
Flow Solver: TAUij

- Compressible Euler
- Explicit RK-4
- Multigrid
- Implicit residual smoothing





Primal compared to coupled iteration



Retardation-Factor = 4

[Özkaya, Gauger, 2008]

Treatment of lift constraint by penalty multiplier method



$$\min_u C_D(y, u) \quad s.t. \quad C_L \geq C_{L, target} \quad and \quad y = G(y, u)$$

Penalty function for lift: $h = (C_{L, target} - C_L), \quad h \leq 0$

Redefine objective function: $f = C_D + \lambda h$

$$\min_u C_D(y, u) + \lambda h \quad ; \quad h \rightarrow 0$$

Update the penalty parameter in each one-shot step k :

$$\lambda_{k+1} = \lambda_k (1 + ch), \quad c > 0$$

$$h > 0 \Rightarrow \lambda \uparrow, \quad h < 0 \Rightarrow \lambda \downarrow$$

A good starting value is: $\lambda_0 = \frac{\|\nabla_u C_D\|}{\|\nabla_u h\|}$

Constrained One-Step One-Shot

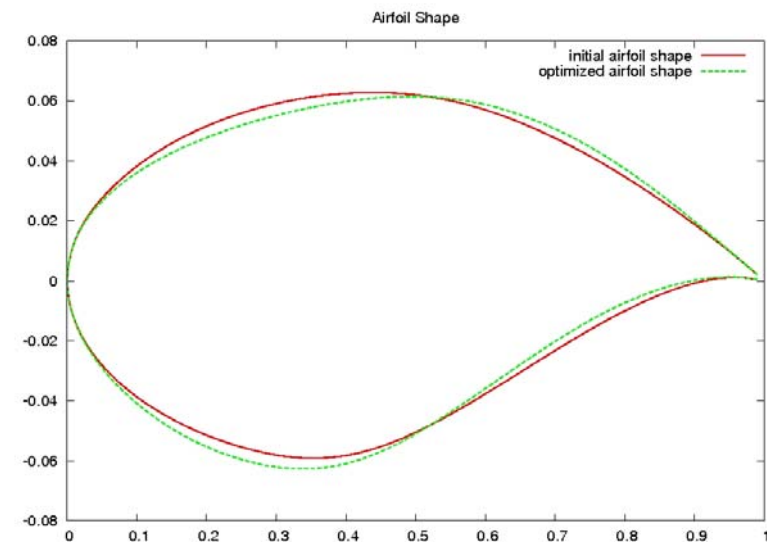
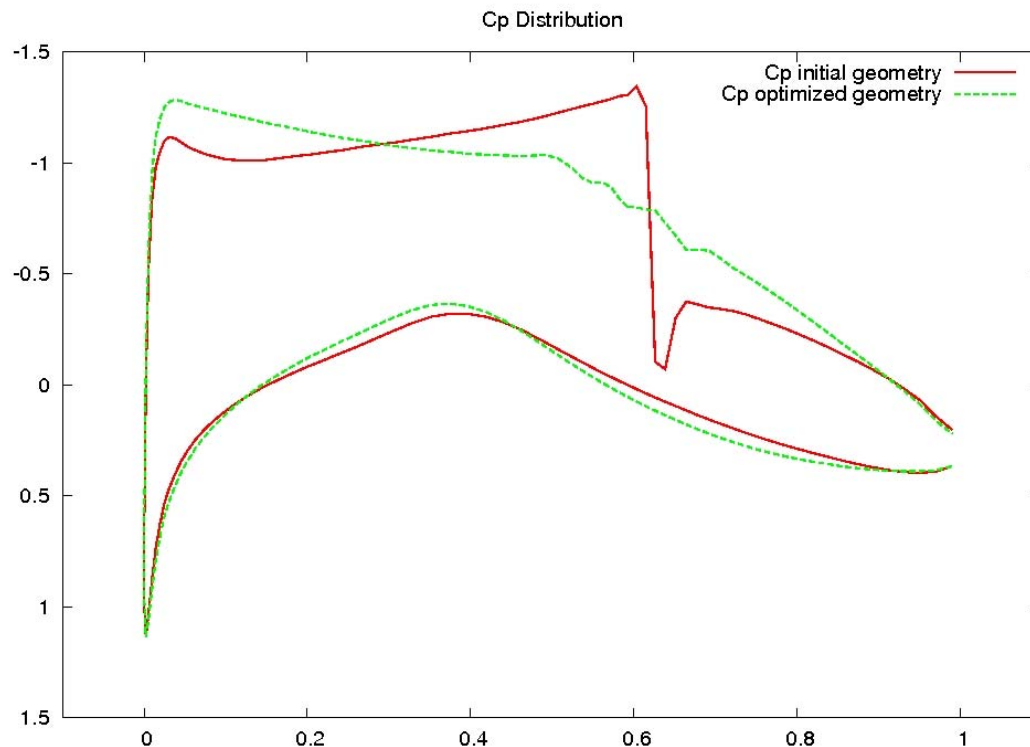


Drag reduction by constant lift

- RAE 2822, $M = 0.73$, $\alpha = 2.0^\circ$
- inviscid flow, mesh 161x33 cells
- 40 design variables (Hicks-Henne)
- One-step one-shot

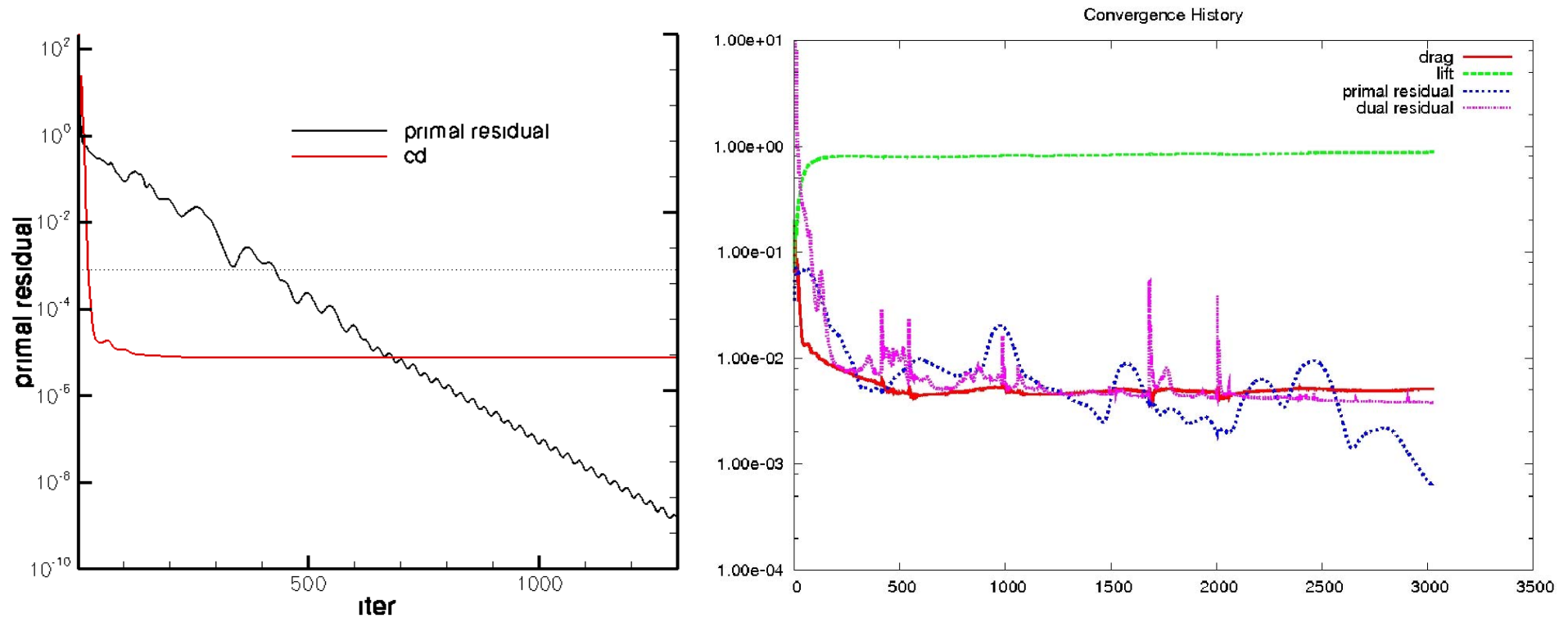
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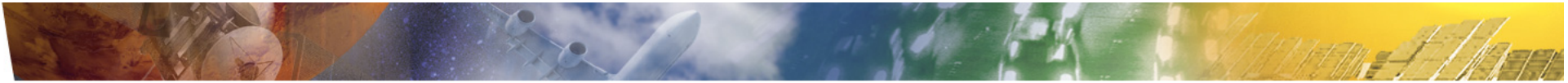


Primal compared to coupled iteration

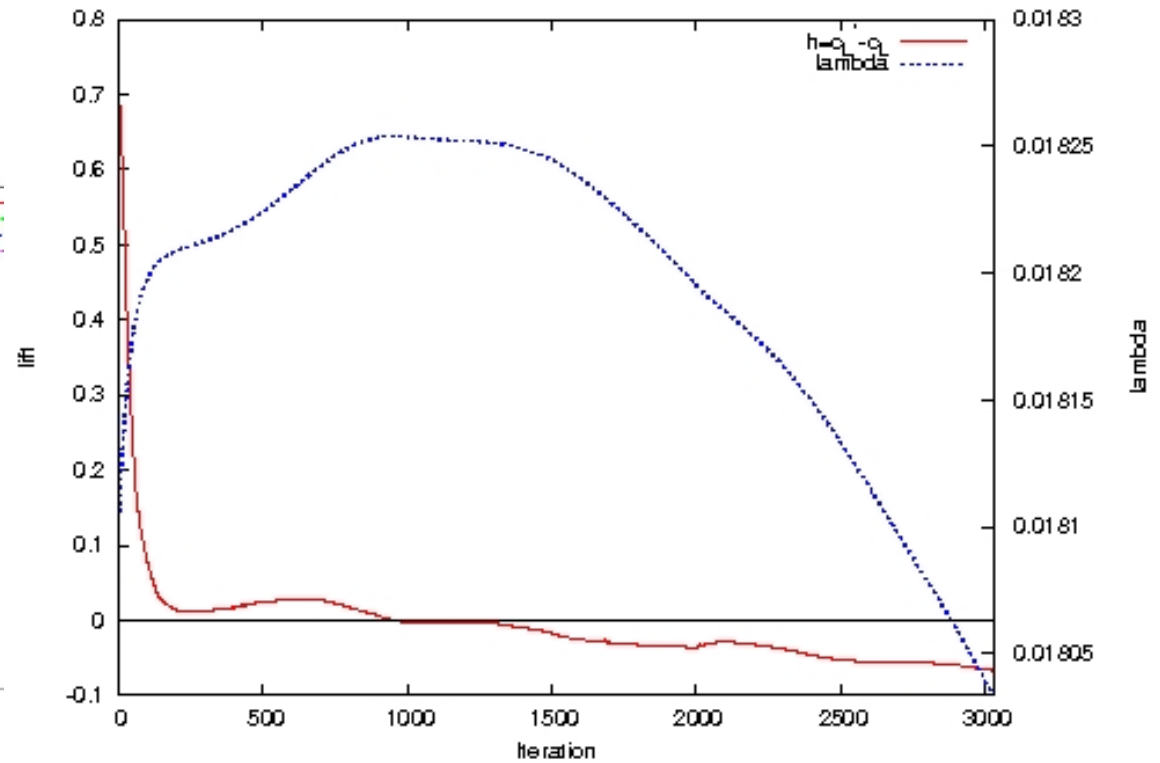
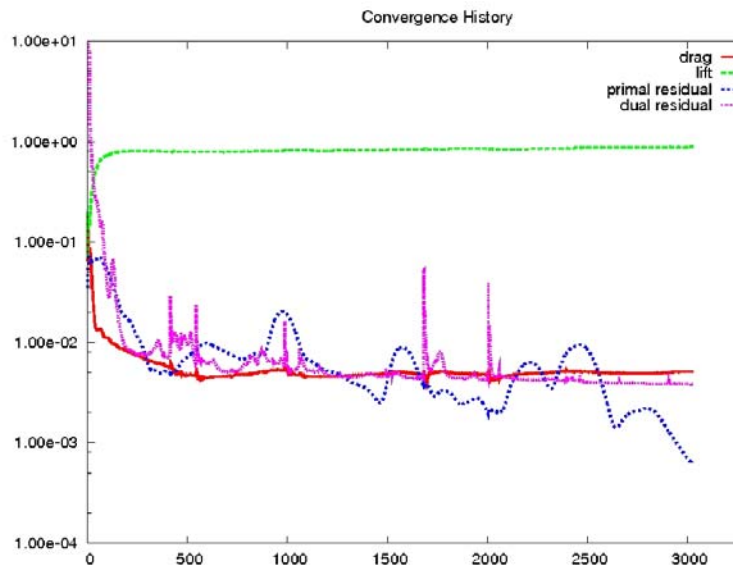


Retardation-Factor = 6

[Gauger, Plocke, 2008]



History of Penalty Multiplier



[Gauger, Plocke, 2008]



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in der Helmholtz-Gemeinschaft

Trier, June 3-5, 2009

PDE Constrained Optimization of Certain and Uncertain Processes

Nico Gauger

Slide 19

Extension to Navier-Stokes (ELAN Code)



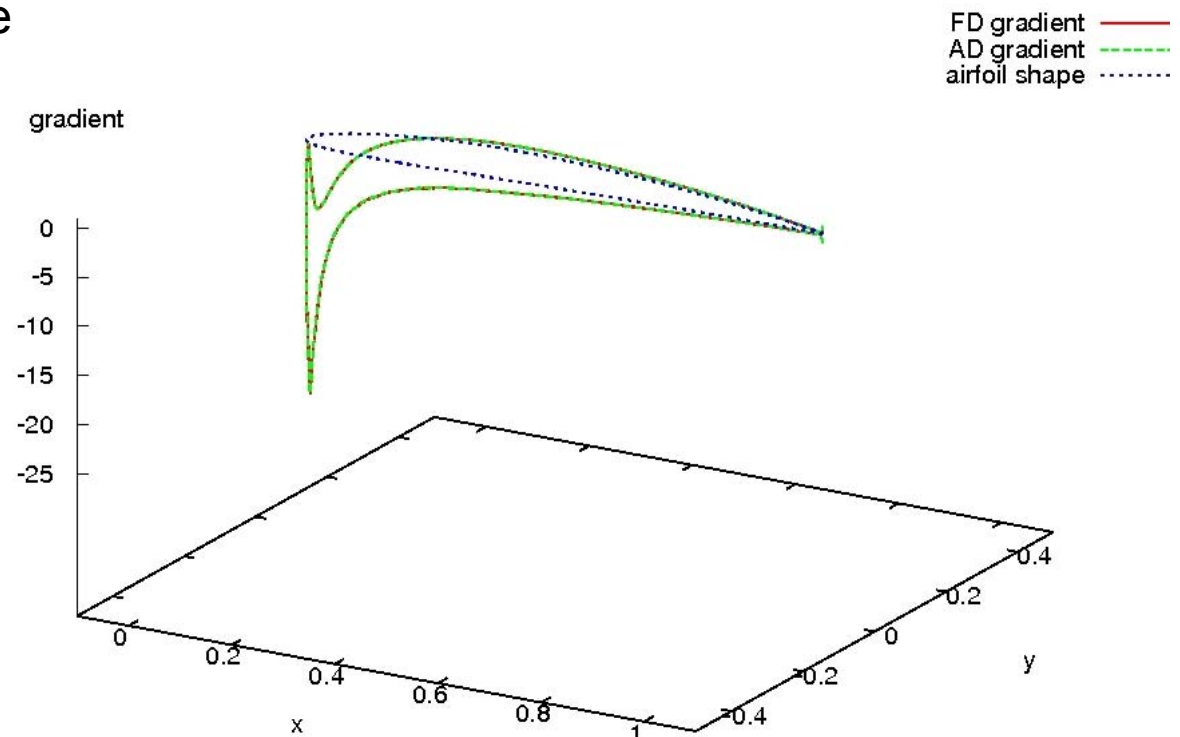
Flow Solver: ELAN (TU Berlin)

- 3D Navier-Stokes (RANS)
- incompressible with pressure correction
- multiblock
- $k-\omega$ (Wilcox) turbulence model (and others)
- Fortran (20.000 lines)

AD Tool: TAPENADE (INRIA)

- source to source
- reverse for **first derivatives**
- tangent on reverse for **second derivatives**

AD-FD Comparison



Extension to Navier-Stokes (ELAN Code)

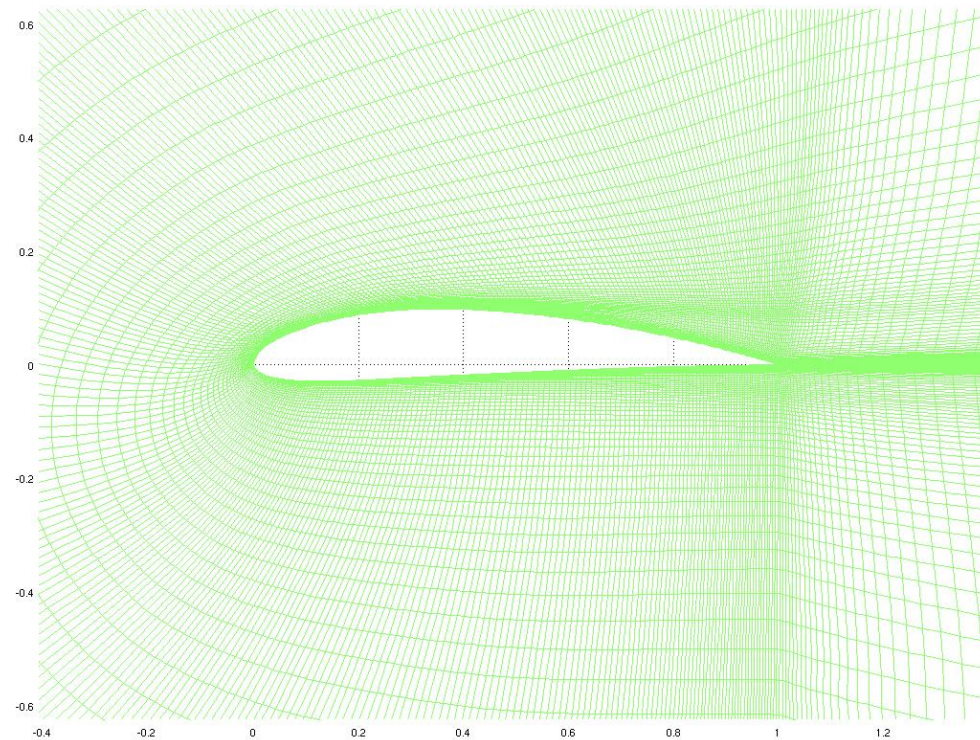
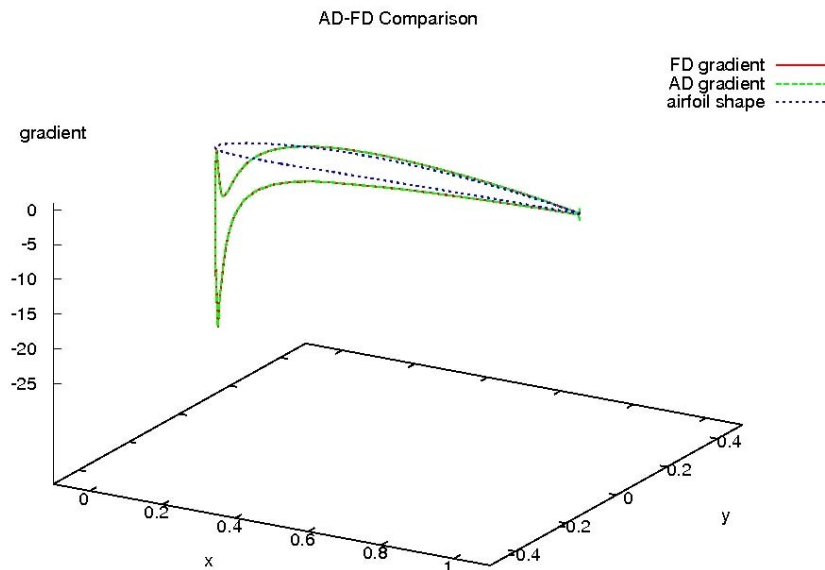


Drag reduction with lift constraint

- NACA 4412
- $Re = 1.000.000$, $\alpha = 5.1^\circ$
- RANS
- k- ω (Wilcox) turbulence model
- 300 surface mesh points

Approaches for Optimization

- one-shot method
- entire design chain differentiated
- gradient smoothing
- penalty multiplier method



Extension to Navier-Stokes (ELAN Code)



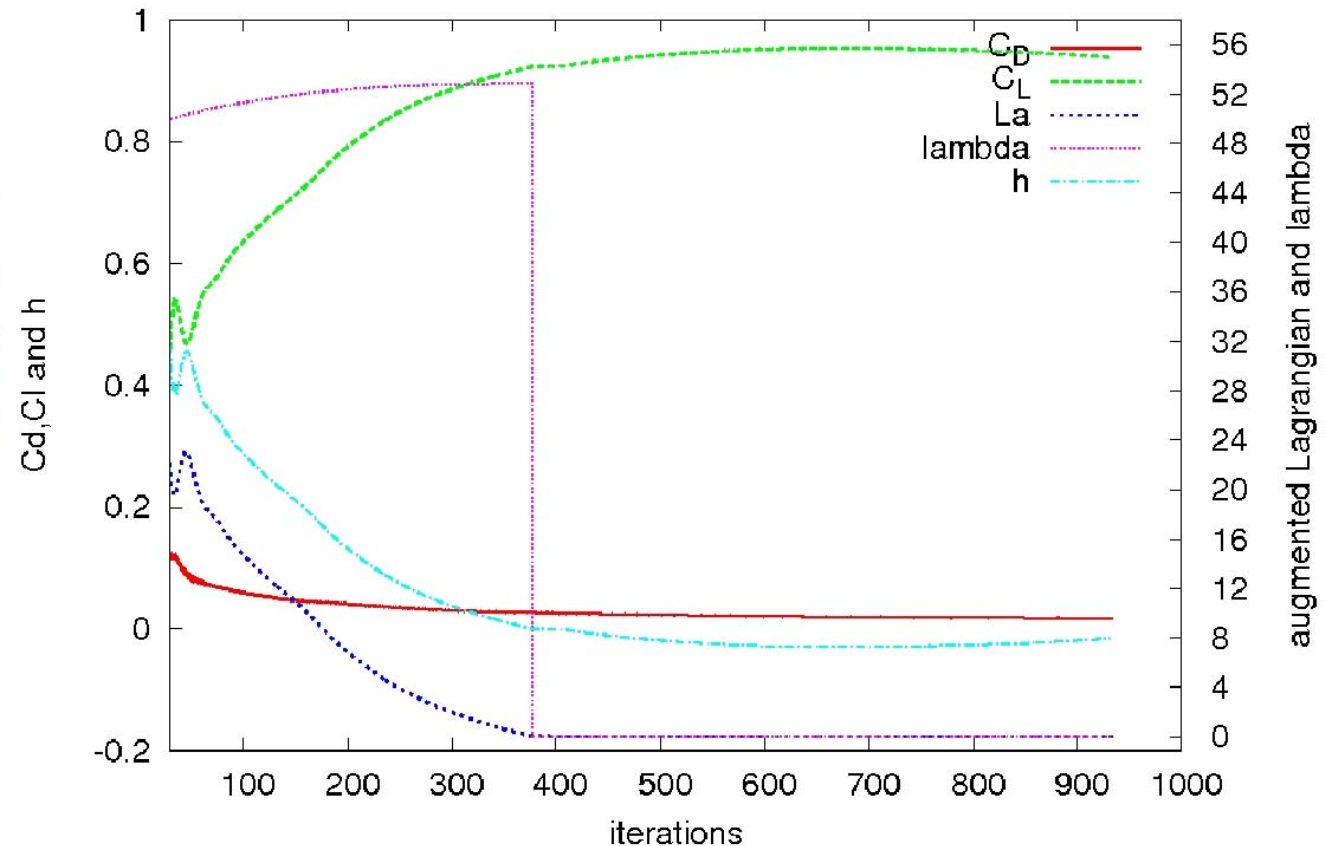
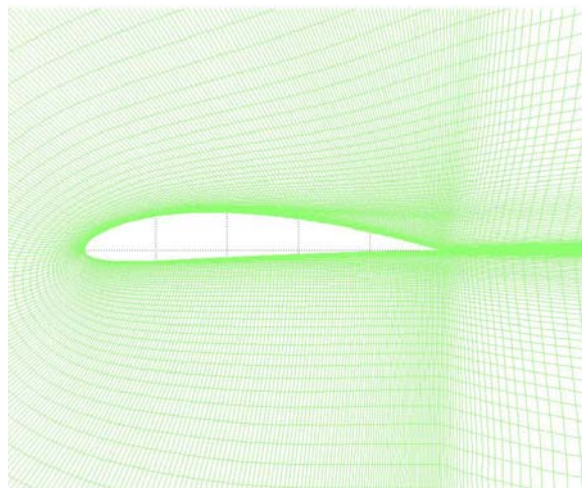
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Approaches for Optimization

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Augmented Lagrangian and aerodynamic coefficients



Extension to Navier-Stokes (ELAN Code)



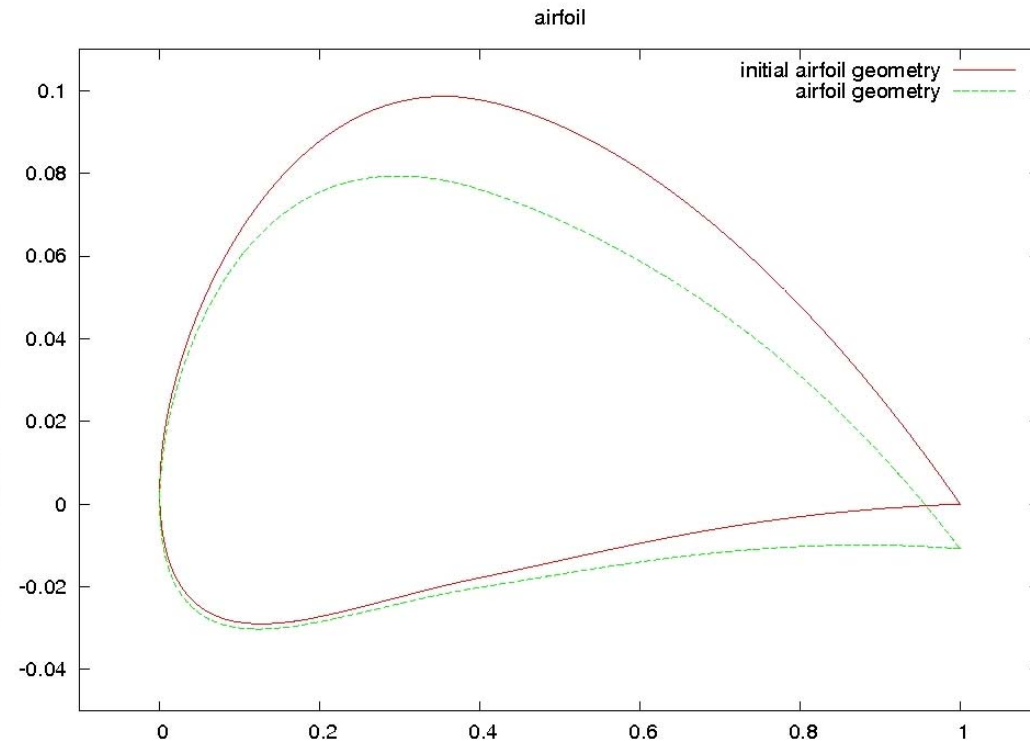
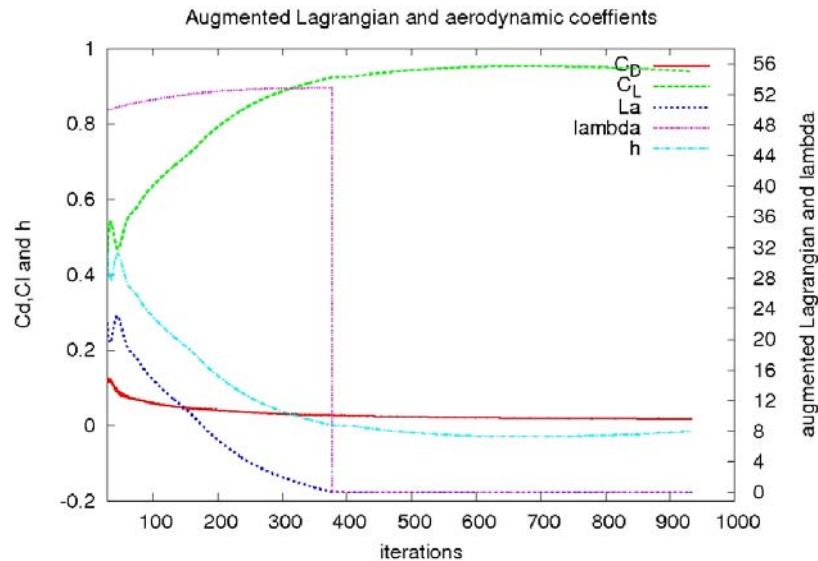
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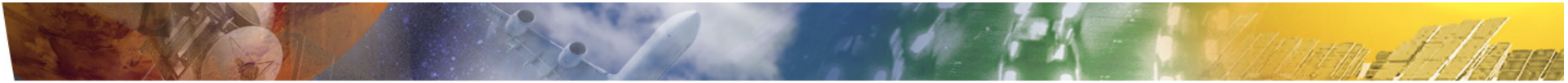
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5% drag reduction





Thanks for your attention!



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